

The top banner features a blue background with white circuit symbols, including a circular node with an 'X' and arrows pointing left and right. The logo 'EDICON' is centered at the top, with 'ED' in black and 'CON' in white on a blue background.

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Electronic Design Innovation
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Cut-off frequency Prediction for MMW Coaxial Interconnects

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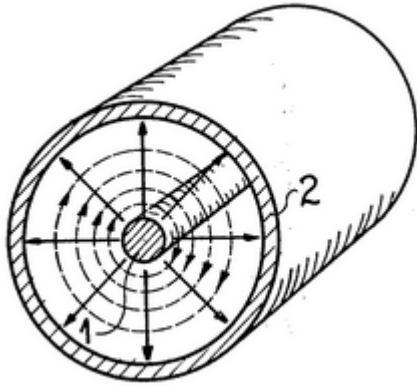
James Broomall, W.L. Gore & Assoc., Inc (retired)

Motivation

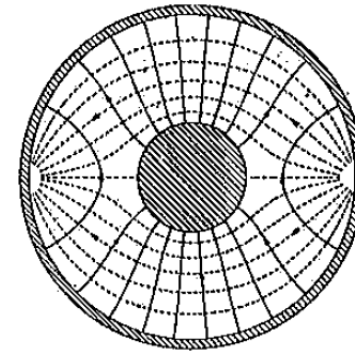
- Knowing the maximum operating frequency of a cable assembly is critical for engineers working at millimeter wave frequencies (e.g. MMW 5G)
- This maximum, or cut-off frequency is considered to be when higher order modes (e.g. the TE_{11} mode) can propagate, robbing signal from the fundamental TEM mode
- Minimizing signal attenuation through the entire frequency range is desired
- The TE_{11} mode frequency and attenuation are both influenced by coax diameter (or size)

Higher order modes in coax

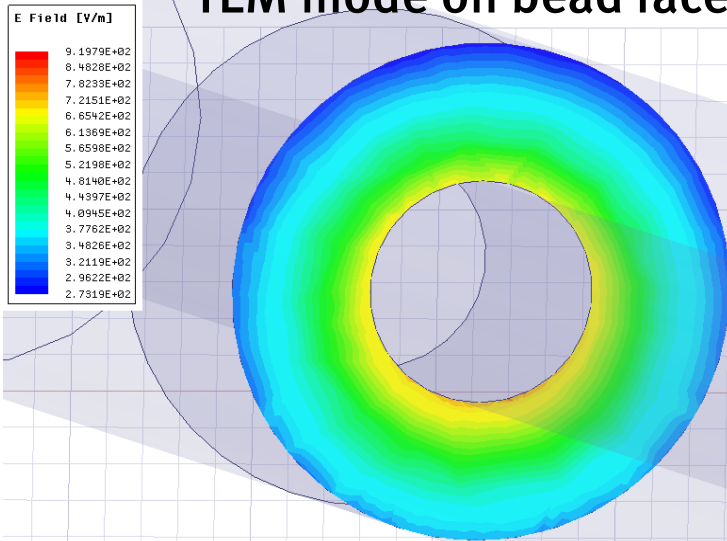
TEM = fundamental mode for coax



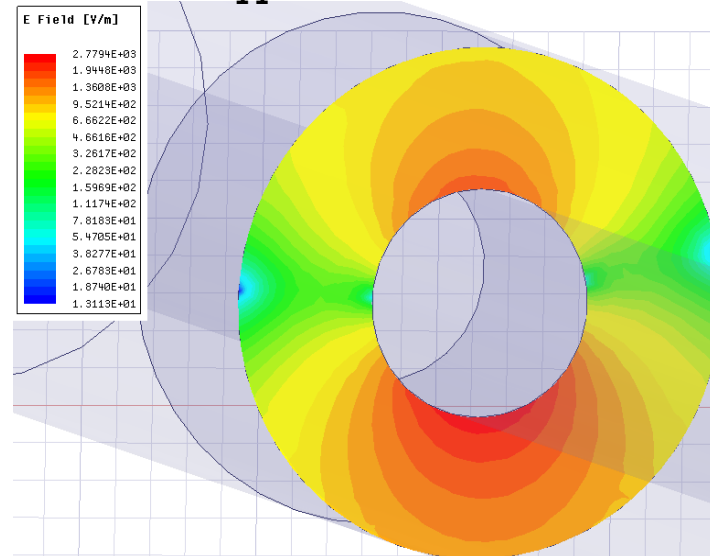
TE₁₁ = first higher order mode encountered in coax



TEM mode on bead face



TE₁₁ mode on bead face



Cutoff frequency for 50Ω airlines

Airline OD (mm)	TE11 cutoff (GHz)	Rated max frequency (GHz)	Derating for connectors
7.0	19.40	18	7%
3.5	38.80	33	15%
2.92	46.51	40	14%
2.4	56.58	50	12%
1.85	73.40	65	11%
1.0	135.80	110	19%

Approximate solution:

$$f_c \approx \frac{190.85}{(d + D)\sqrt{\epsilon_r}} \text{ (GHz)}$$

d and D are inner and outer diameters (mm)
 ϵ_r is the effective dielectric constant of the section

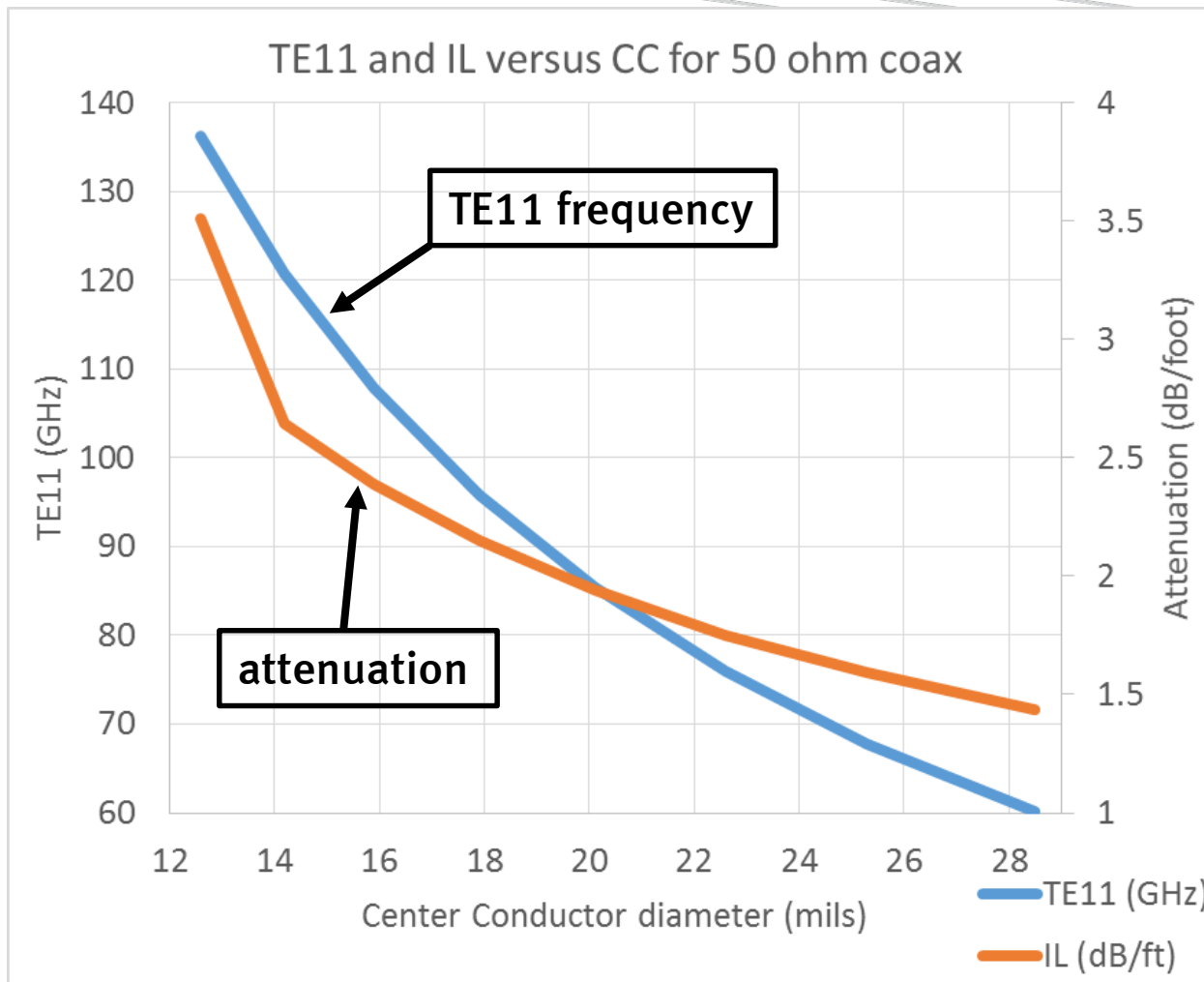
Exact solution using characteristic Bessel equation:

$$J_1'(k_c b) N_1'(k_c a) - J_1'(k_c a) N_1'(k_c b) = 0$$

where; a = Inner radius, b = Outer radius

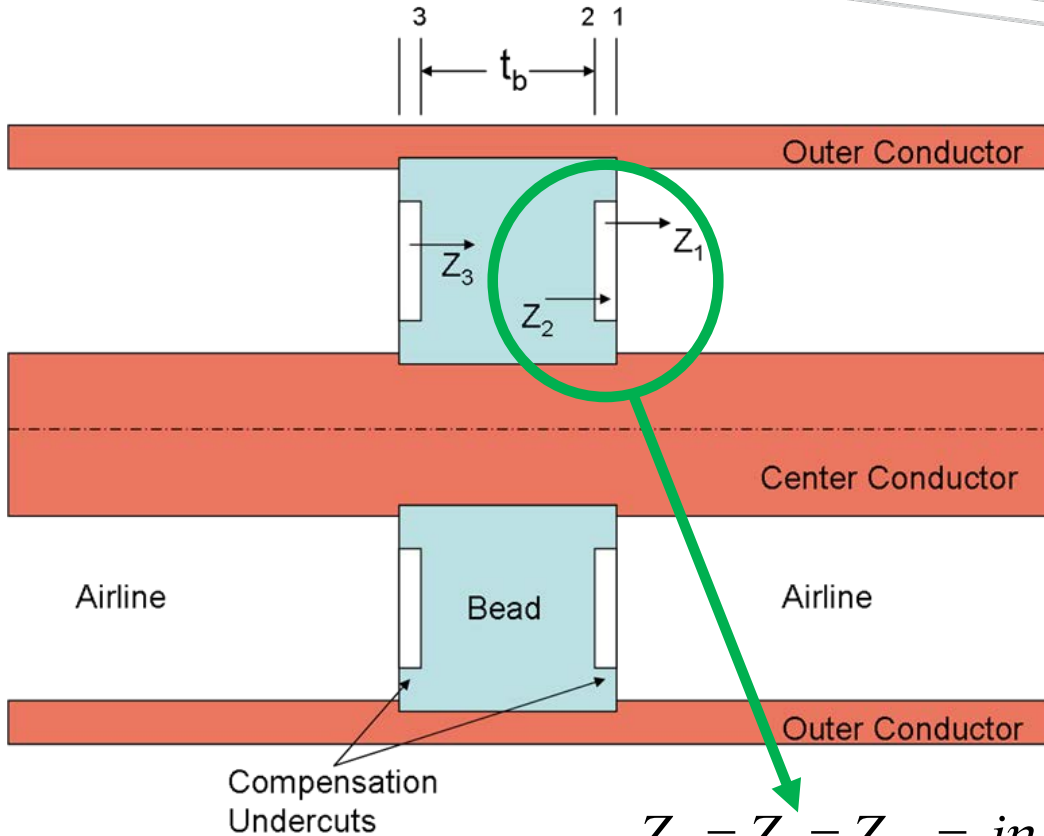
$$k_c = 2\pi\sqrt{\epsilon_r} \frac{f_c}{c_0}$$

Cutoff frequency versus attenuation



Calculate effective TE₁₁ modes beads

Gilmore, The General Radio Experimenter, 1966



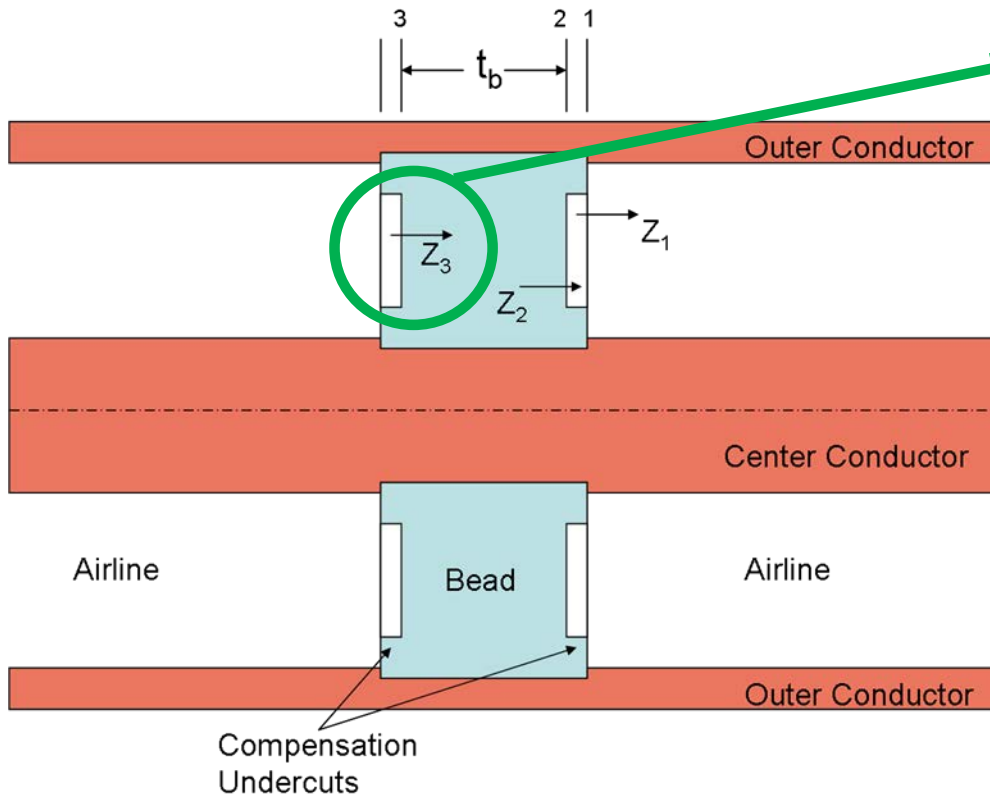
Perform transmission line calculations in terms of TE wave impedance and propagation constant

$$Z_2 = Z_1 = Z_{0a} = j\eta_0 \frac{f}{f_{ca}} \frac{1}{\sqrt{1 - \left(\frac{f}{f_{ca}}\right)^2}} \quad \text{for } f < f_{ca}$$

where; $\eta_0 = 376.7$ ohms

$f_{ca} = \text{TE}_{11}$ frequency of the infinite airline section

Calculate effective TE₁₁ modes beads



$$Z_3 = Z_{0b} \frac{Z_{0a} + Z_{ob} \tanh(\gamma_b t_b)}{Z_{0b} + Z_{oa} \tanh(\gamma_b t_b)}$$

where; $Z_{ob} = \eta_b \frac{1}{\sqrt{1 - \left(\frac{f_{cb}}{f}\right)^2}}$

$$\gamma_b = jk_b \sqrt{1 - \left(\frac{f_{cb}}{f}\right)^2}$$

$$\eta_b = \frac{376.7}{\sqrt{\epsilon_{rb}}}$$

$$k_b = 2\pi \sqrt{\epsilon_{rb}} \frac{f}{c_0}$$

$t_b =$ Length of bead section

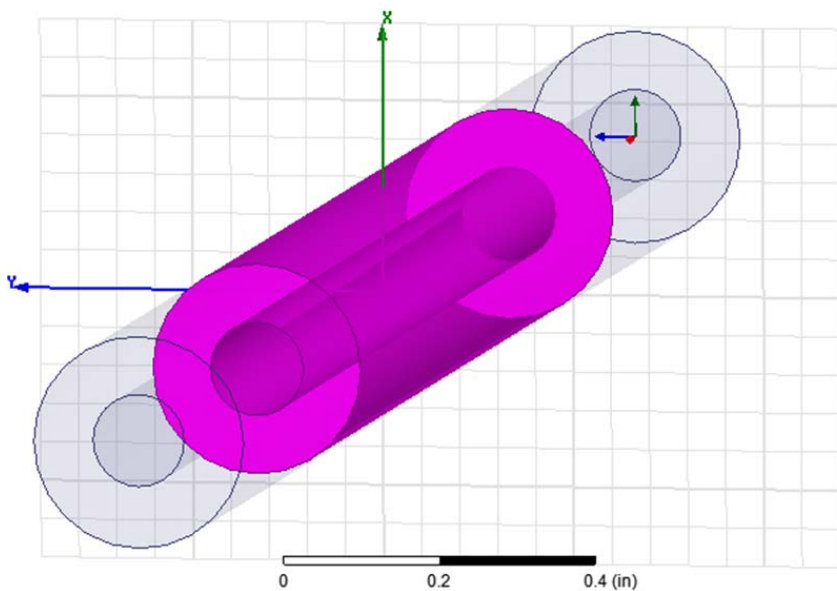
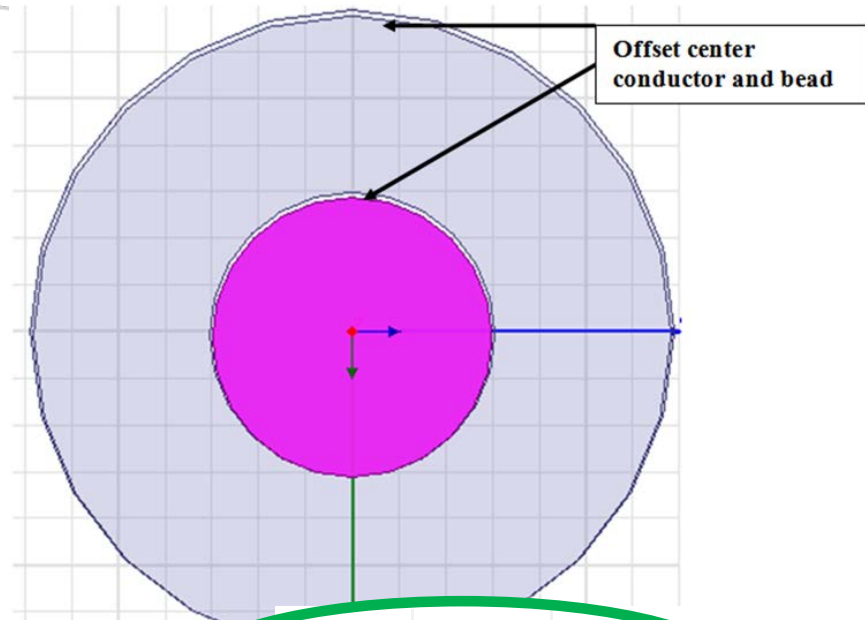
Resonance conditions occurs when:

$$Z_3 = Z_{0a}^*$$

Effective TE_{11} mode in coax support beads

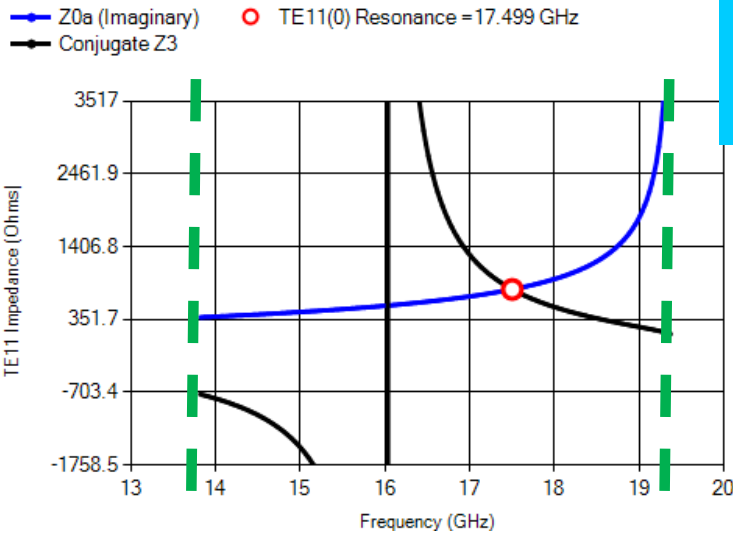
- TE_{11} mode resonance(s) will occur at the frequencies where $Z_3 = Z_{0a}^*$
- Multiple resonances can occur for the TE_{11} mode, based on bead length
- The bead is now the determining factor for the maximum operating frequency of the coax assembly
- A simple experiment can be run to test the theory
 - Use various lengths of a PTFE bead inserted into a 7mm airline

PTFE bead with 7mm airline experiment

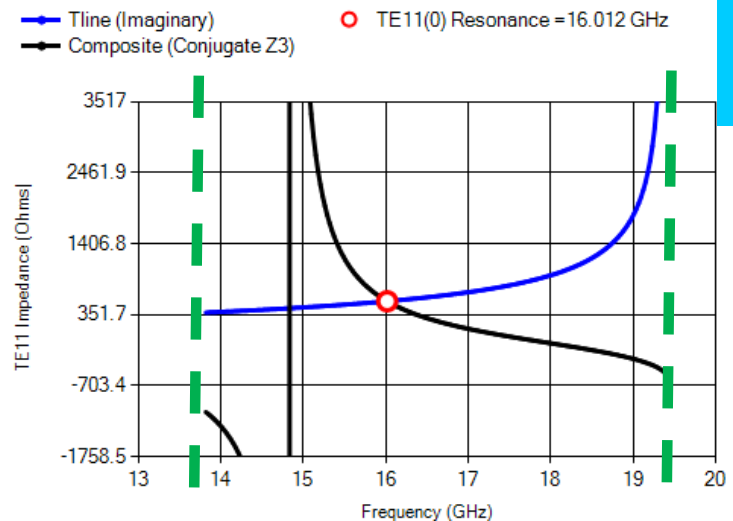
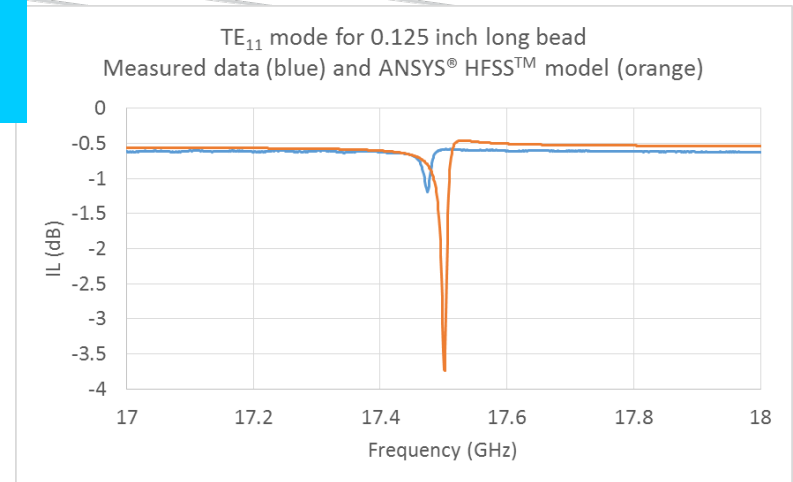


Mode	Bead	T-Line
TE11	13.8	19.4
TE21	27.0	38.0
TE31	39.4	55.4
TM01	53.3	75.0
TE01	55.1	77.6
TM11	55.1	77.6
TE12	57.4	80.7
TM21	60.2	84.6
TE22	63.7	89.6

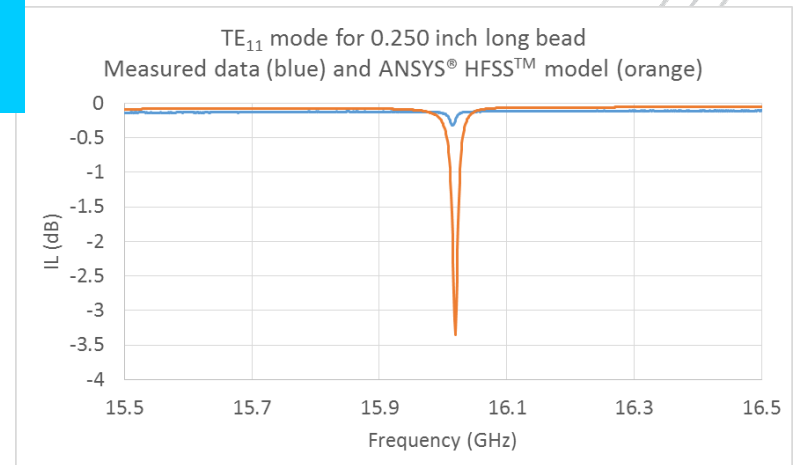
PTFE bead with 7mm airline experiment



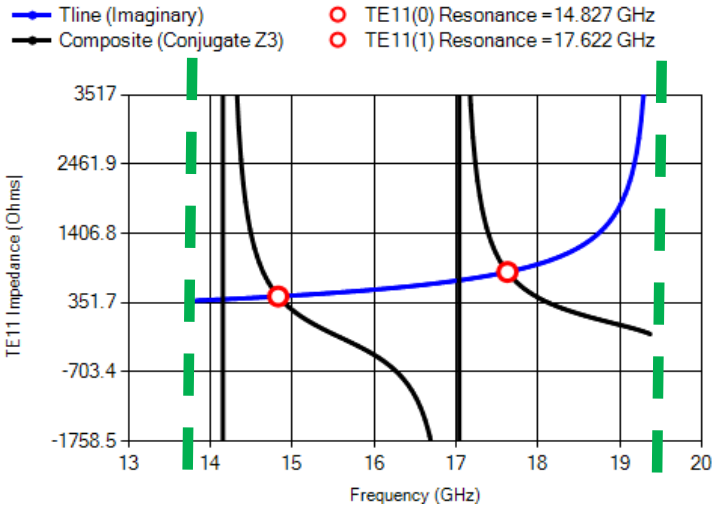
**0.125 inch
long bead**



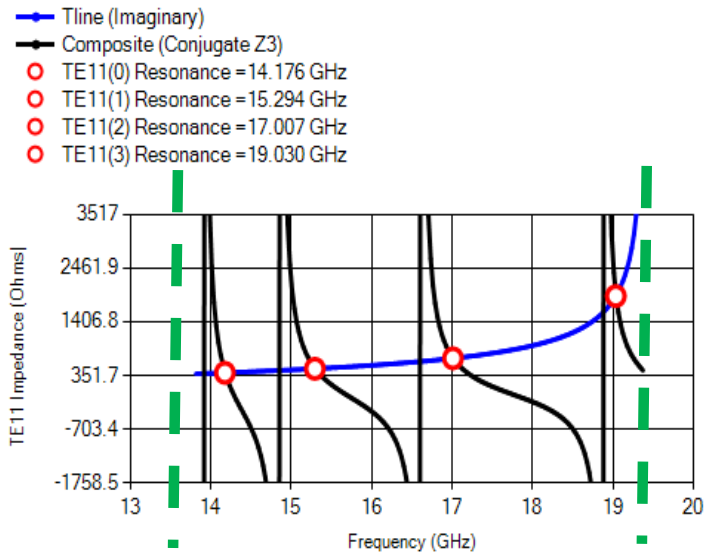
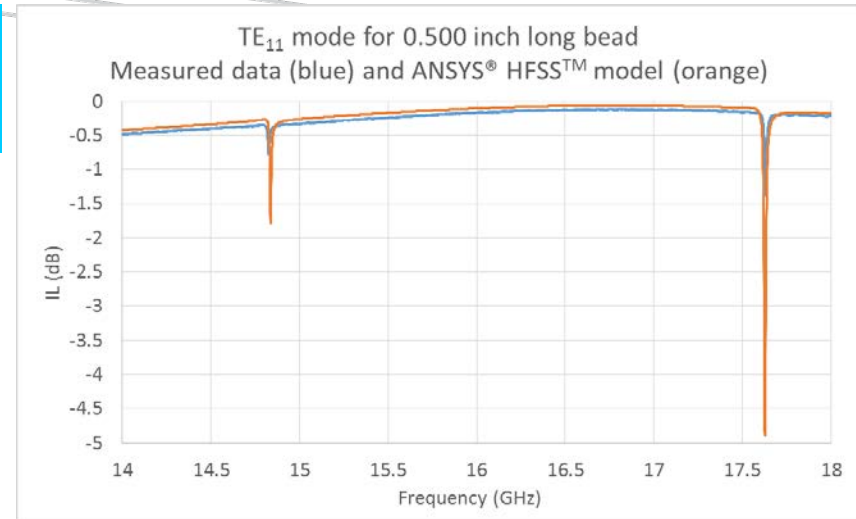
**0.250 inch
long bead**



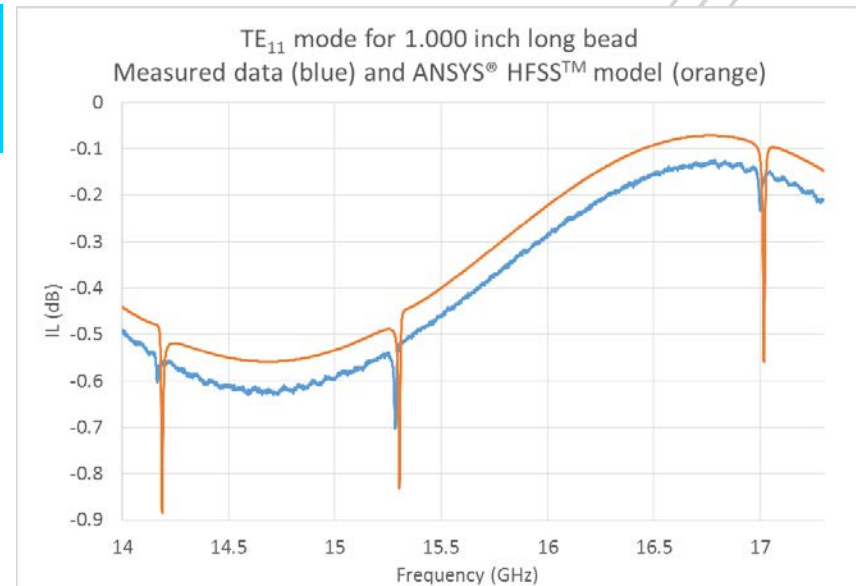
PTFE bead with 7mm airline experiment



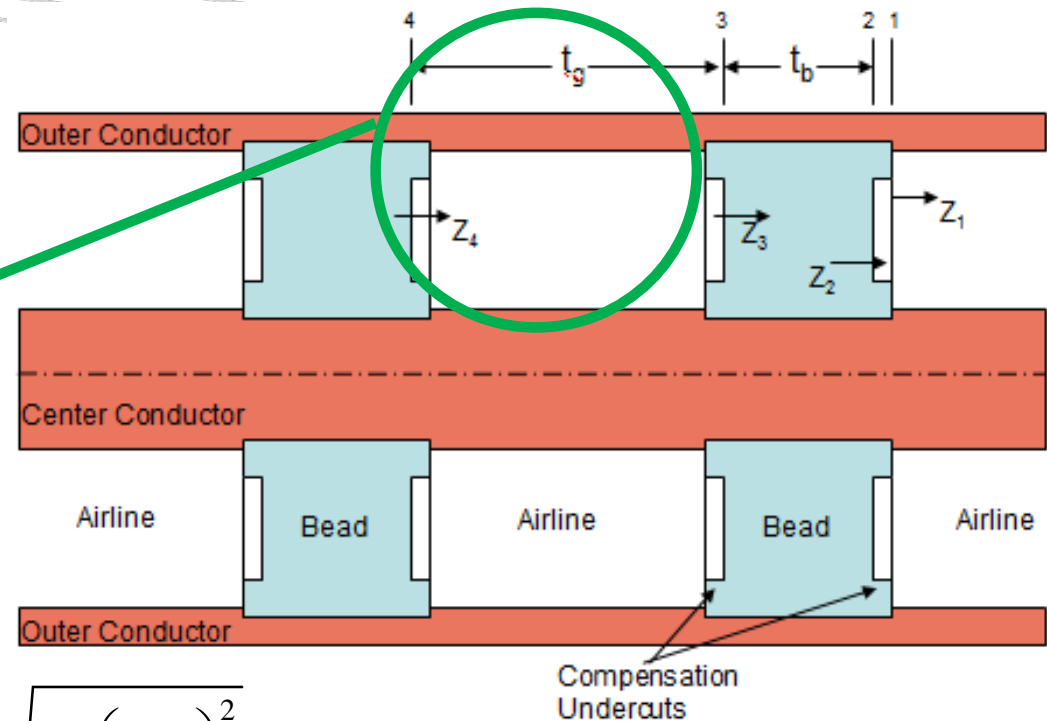
0.5 inch long bead



1.0 inch long bead



Dual beads within an airline



$$Z_4 = Z_{0g} \frac{Z_3 + Z_{0g} \tanh(\gamma_g t_g)}{Z_{0g} + Z_3 \tanh(\gamma_g t_g)}$$

where; $Z_{0g} = Z_{0a}$; $\gamma_g = \gamma_a = k_a \sqrt{1 - \left(\frac{f}{f_{ca}}\right)^2}$

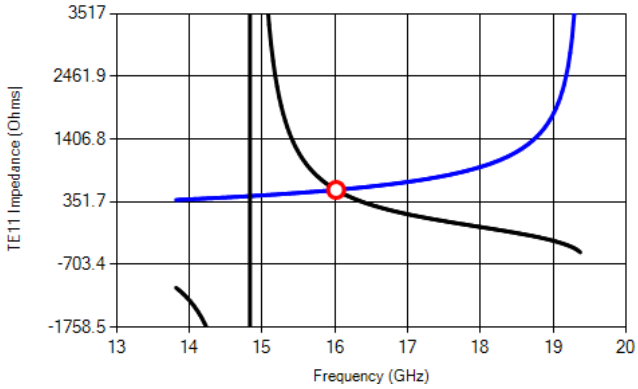
Resonance conditions occurs when:

$$Z_4 = Z_3^*$$

Dual PTFE beads within 7mm airline

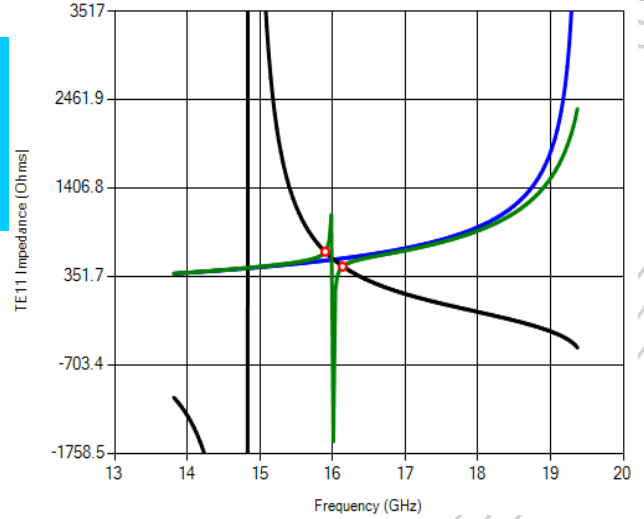
0.250 inch long single bead

- Tline (Imaginary)
- Composite (Conjugate Z3)
- TE11(0) Resonance = 16.012 GHz



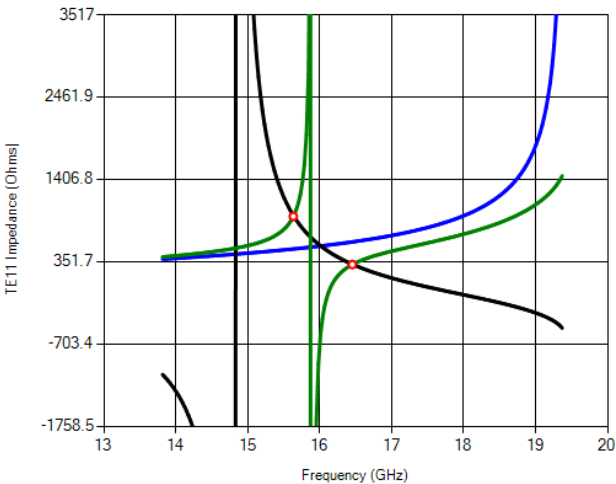
(2x) 0.250 beads, 0.5 inch apart

- Tline (Imaginary)
- Composite (Conjugate Z3)
- Gap Space (Imaginary Z4)
- TE11(0:Low) Resonance = 15.896 GHz
- TE11(0:High) Resonance = 16.139 GHz



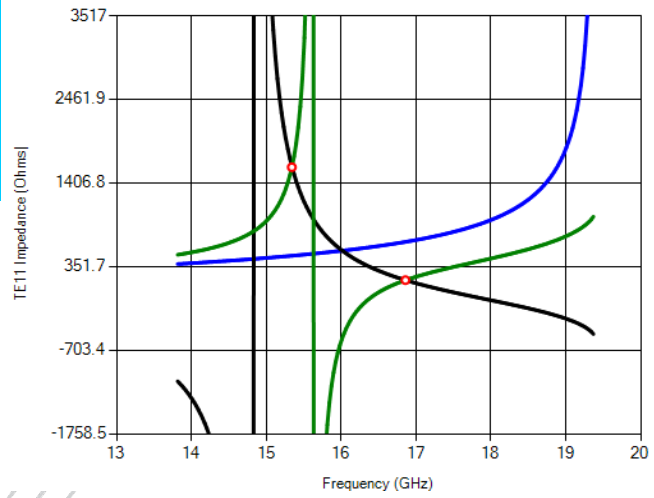
(2x) 0.250 beads, 0.250 inch apart

- Tline (Imaginary)
- Composite (Conjugate Z3)
- Gap Space (Imaginary Z4)
- TE11(0:Low) Resonance = 15.636 GHz
- TE11(0:High) Resonance = 16.455 GHz



(2x) 0.250 beads, 0.125 inch apart

- Tline (Imaginary)
- Composite (Conjugate Z3)
- Gap Space (Imaginary Z4)
- TE11(0:Low) Resonance = 15.344 GHz
- TE11(0:High) Resonance = 16.857 GHz



Conclusions:

- Important to understand TE_{11} mode resonant conditions in order to determine the max operating frequency of coax assembly:
 - Use transmission line calculation approach
 - Using TE wave impedance and prop const.
 - Simulate using ANSYS® HFSS™ software (or equiv.)
 - Introduce slight asymmetries
 - Measure the assembly to validate the lowest TE_{11} resonant frequency