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# Cut-off frequency Prediction for MMW Coaxial Interconnects

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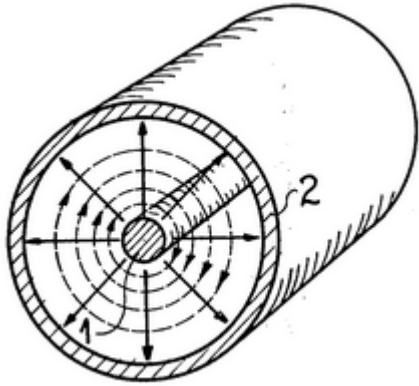
James Broomall, W.L. Gore & Assoc., Inc (retired)

# Motivation

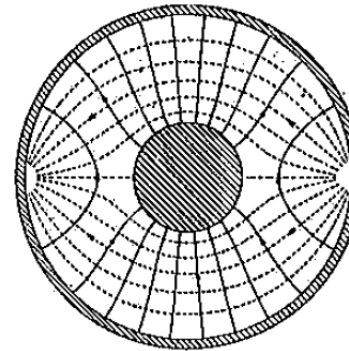
- Knowing the maximum operating frequency of a cable assembly is critical for engineers working at millimeter wave frequencies (e.g. MMW 5G)
- This maximum, or cut-off frequency is considered to be when higher order modes (e.g. the  $TE_{11}$  mode) can propagate, robbing signal from the fundamental TEM mode
- Minimizing signal attenuation through the entire frequency range is desired
- The  $TE_{11}$  mode frequency and attenuation are both influenced by coax diameter (or size)

# Higher order modes in coax

TEM = fundamental mode for coax

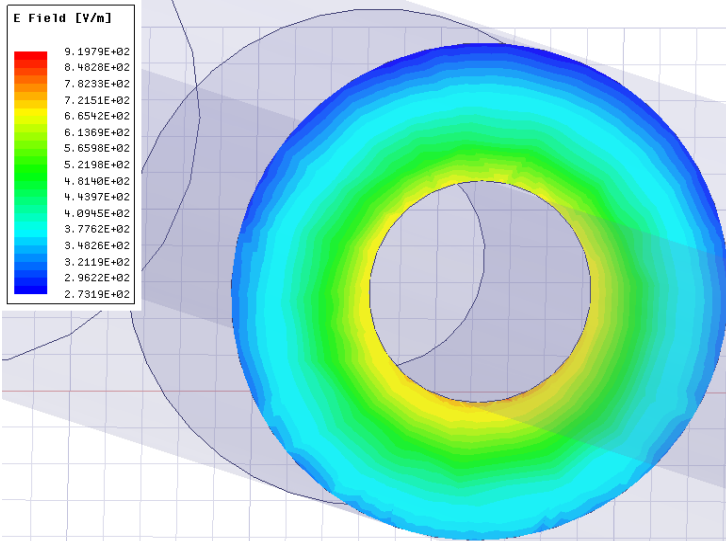


$TE_{11}$  = first higher order mode encountered in coax

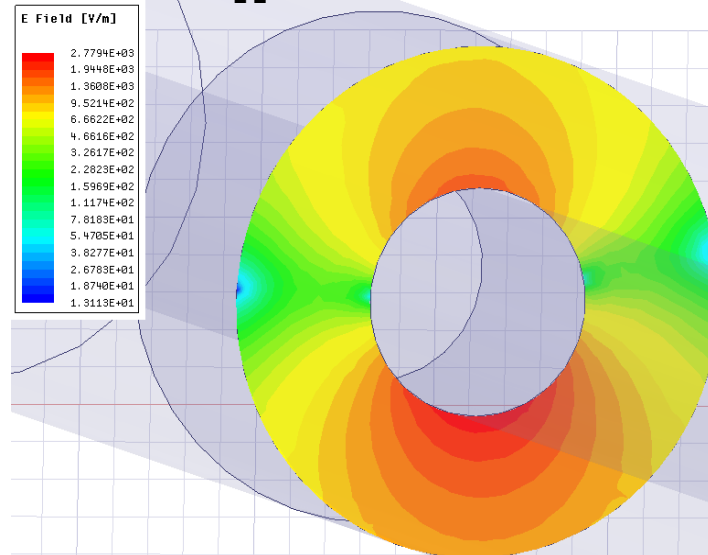


*Excited by asymmetries in cross section*

TEM mode on bead face



$TE_{11}$  mode on bead face



# Cut-off frequency for 50Ω air interfaces

Approximate solution:

$$f_c \approx \frac{190.85}{(d + D)\sqrt{\epsilon_r}} \text{ (GHz)}$$

$d$  and  $D$  are inner and outer diameters (mm)

$\epsilon_r$  is the effective dielectric constant of the section

Airline OD (mm)	$f_c$ (TE <sub>11</sub> ) cut-off (GHz)	Rated max frequency (GHz)	Derating for support beads
7.0	19.40	18	7%
3.5	38.80	33	15%
2.92	46.51	40	14%
2.4	56.58	50	12%
1.85	73.40	65	11%
1.0	135.80	110	19%

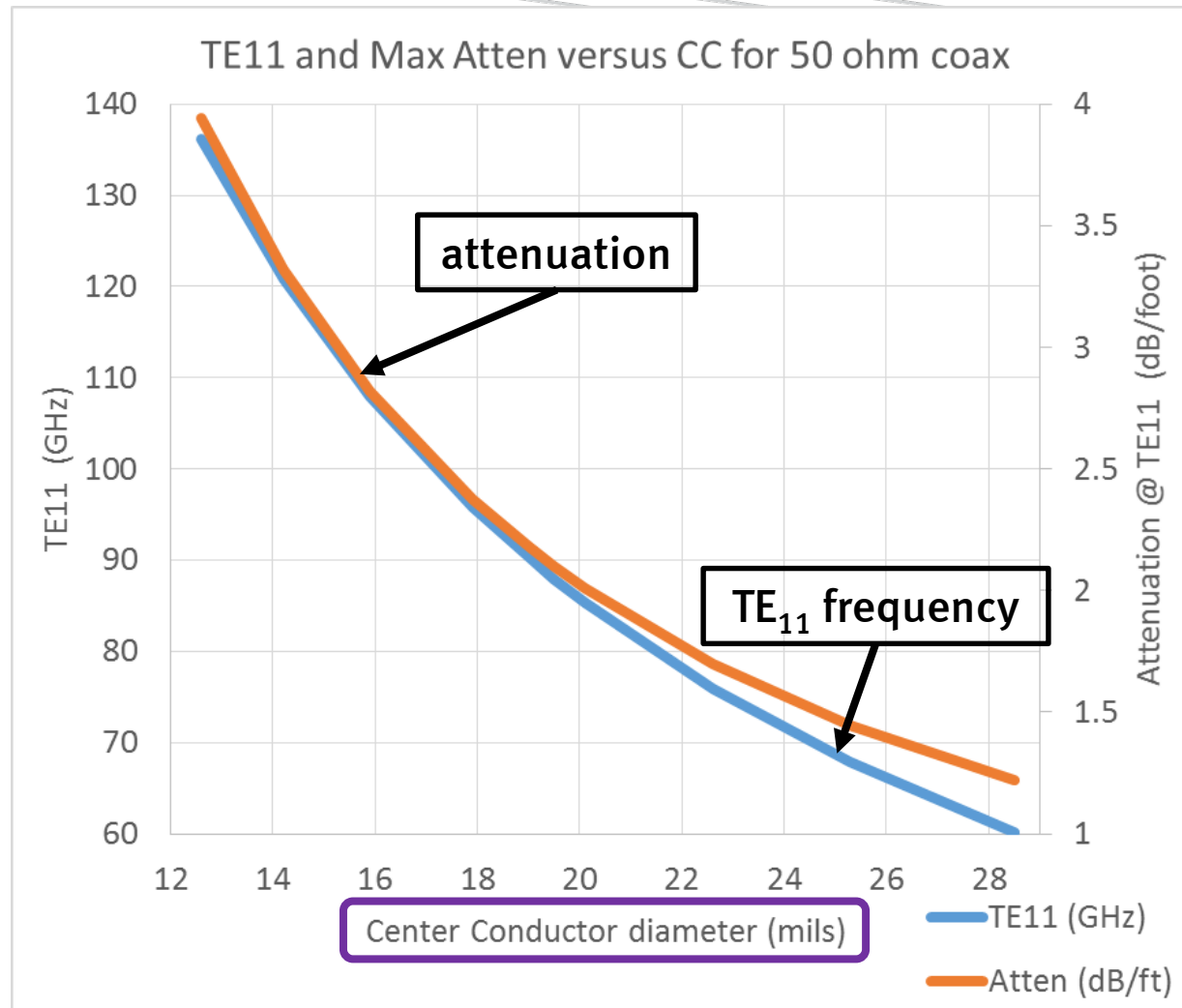
Exact solution using characteristic

Bessel equation (first root):  $J_1'(k_c b)Y_1'(k_c a) - J_1'(k_c a)Y_1'(k_c b) = 0$

where;  $a$  = Inner radius,  $b$  = Outer radius

$$k_c = 2\pi\sqrt{\epsilon_r} \frac{f_c}{c_0}$$

# Cut-off frequency and attenuation of coax



# Cut-off frequency and attenuation of coax

**1.0mm (110 GHz)**

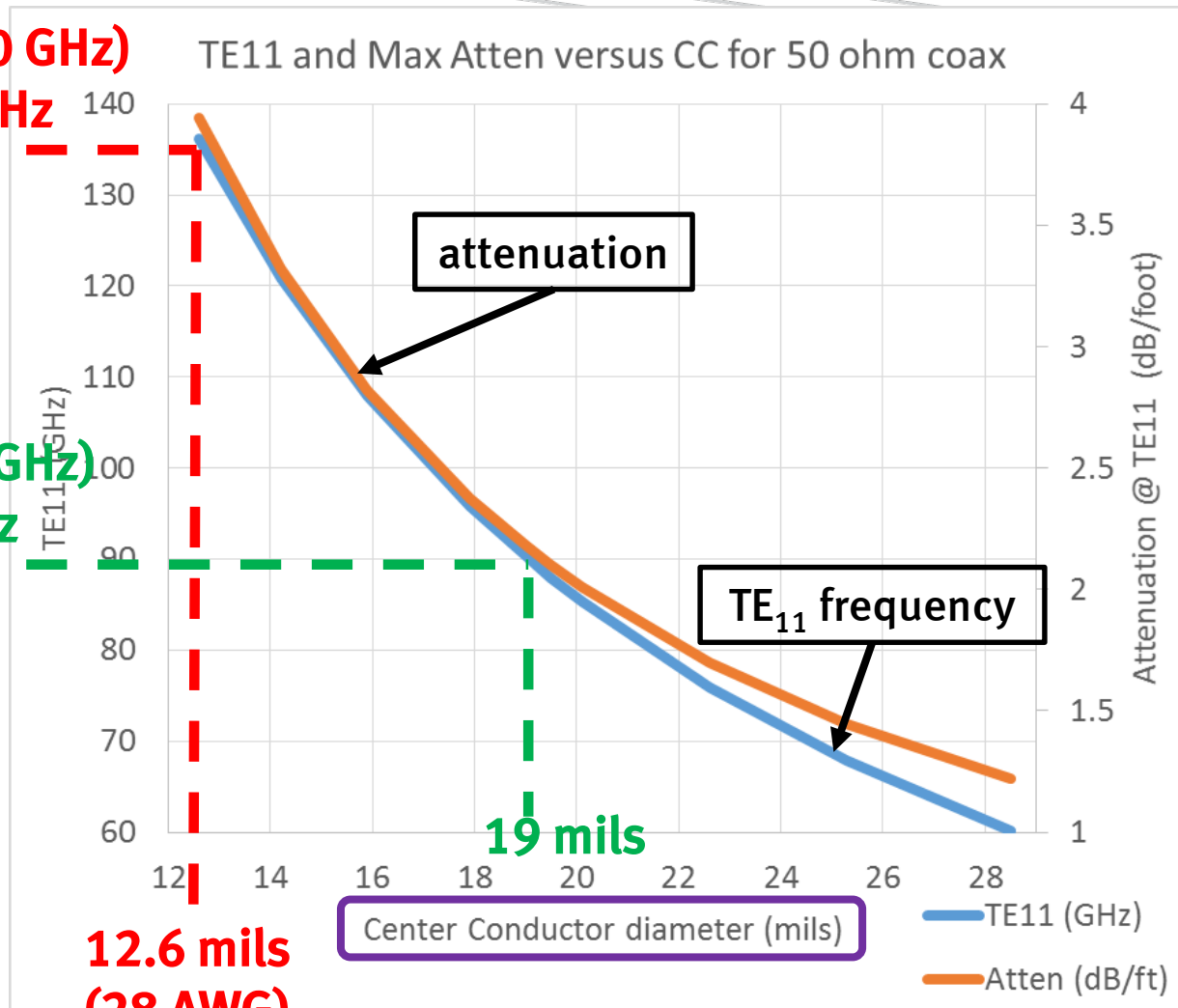
**$TE_{11}=136$  GHz**

**1.5mm (80 GHz)**

**$TE_{11}=90$  GHz**

**12.6 mils  
(28 AWG)**

**19 mils**



# Cut-off frequency and attenuation of coax

**1.0mm (110 GHz)**

**$TE_{11}=136$  GHz**

**3 dB/ft @ 80 GHz**

**1.5mm (80 GHz)**

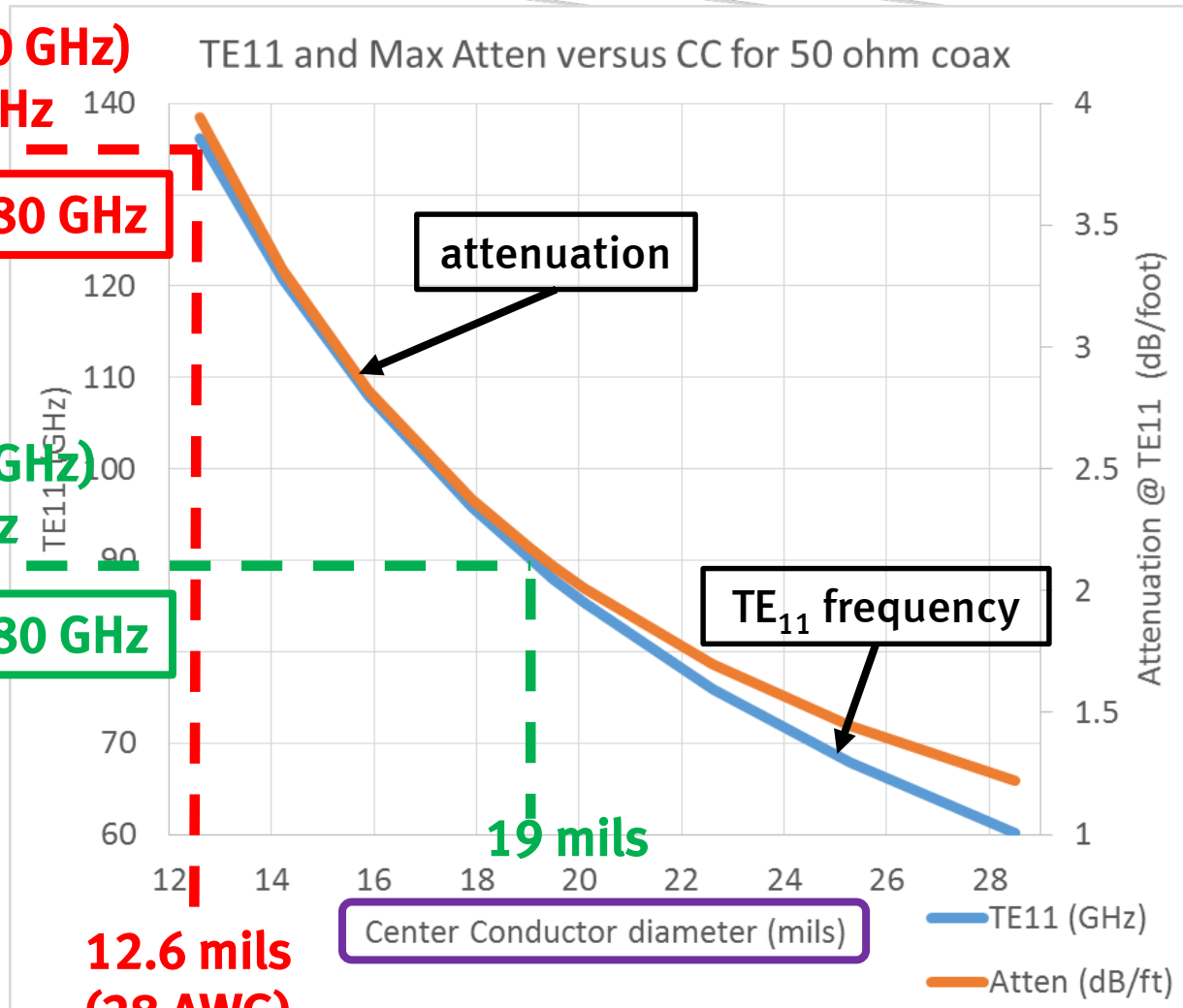
**$TE_{11}=90$  GHz**

**2 dB/ft @ 80 GHz**

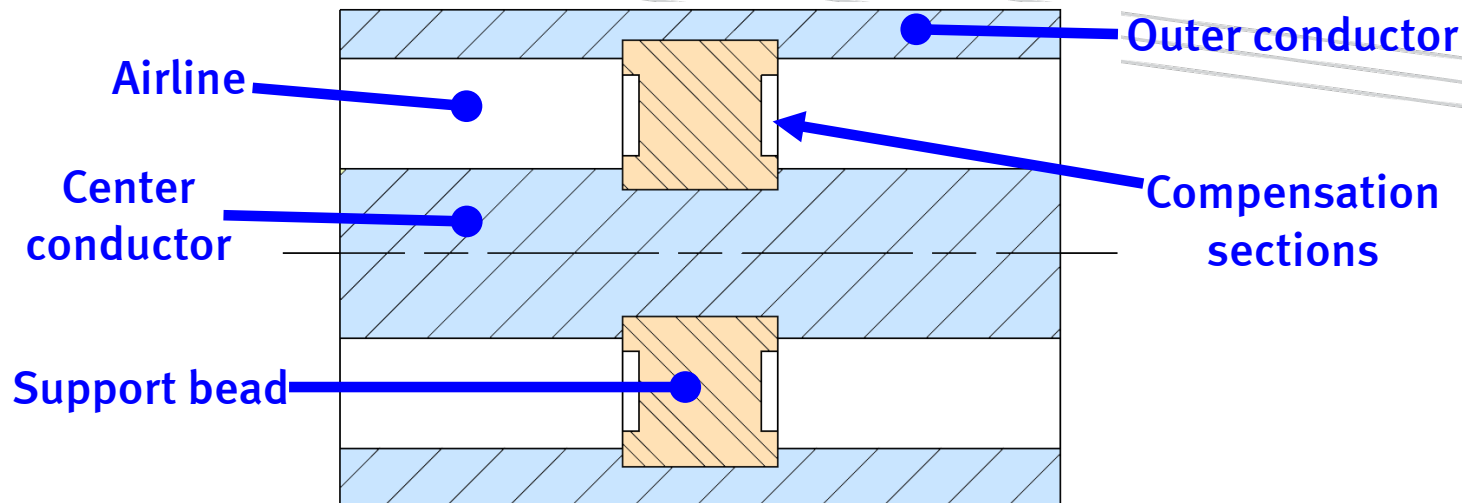
**12.6 mils  
(28 AWG)**

**19 mils**

TE11 and Max Atten versus CC for 50 ohm coax



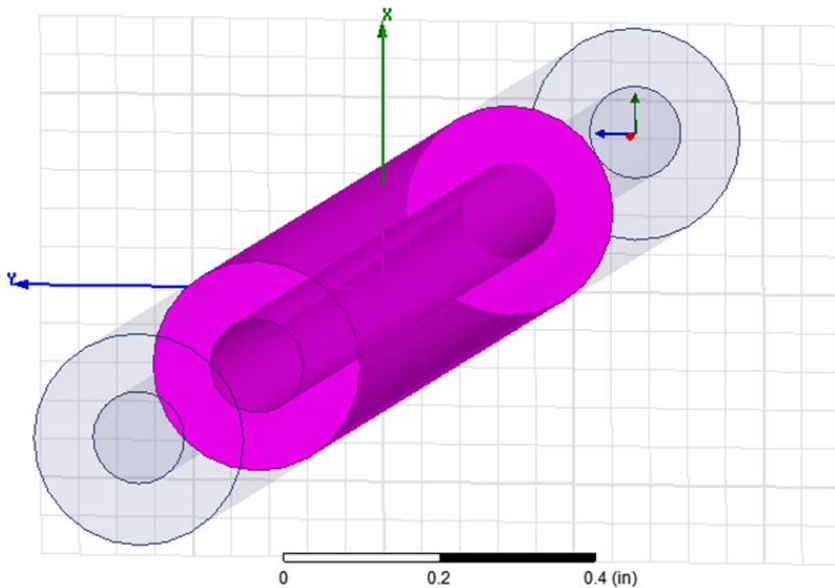
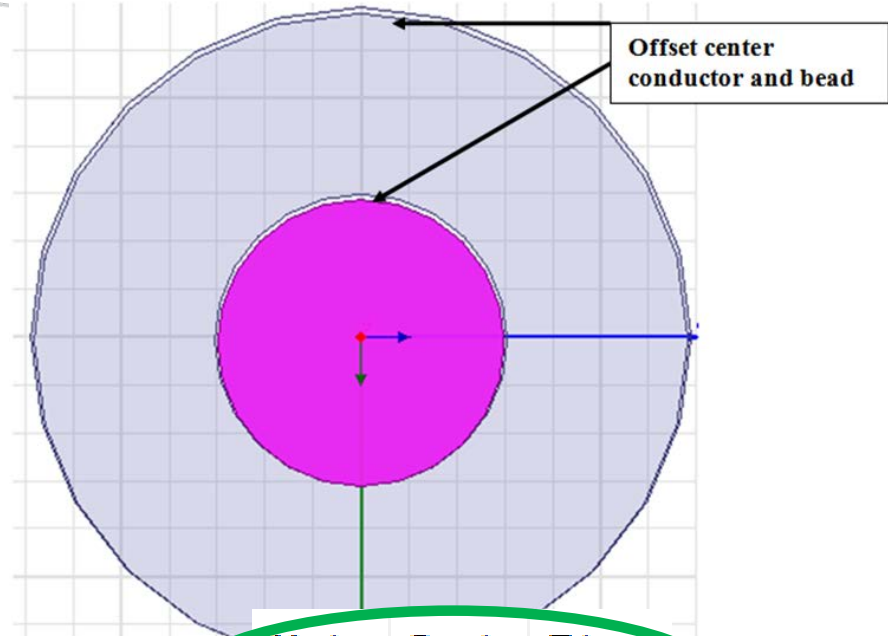
# Support beads for connectors



- Bead supports CC radially and longitudinally and has the same nominal impedance as airline
- $TE_{11}$  mode frequency in bead section is lower than in airline
- Effective cut-off frequency of bead will end up somewhere between  $TE_{11}$  of bead and airline
  - Resonance occurs when impedance of TE waves are complex conjugates at boundaries

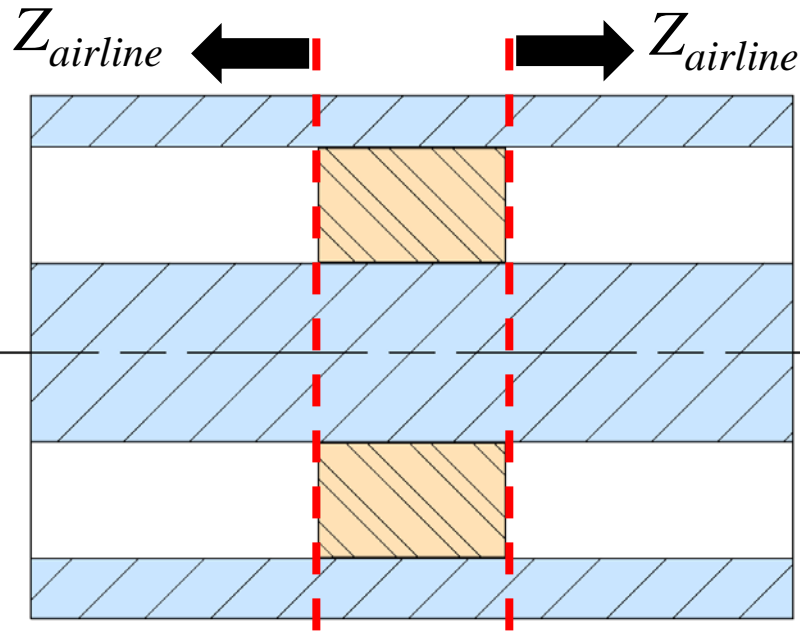


# Example: PTFE beads in 7mm airline



Mode	Bead	T-Line
TE11	13.8	19.4
TE21	27.8	38.0
TE31	39.4	55.4
TM01	53.3	75.0
TE01	55.1	77.6
TM11	55.1	77.6
TE12	57.4	80.7
TM21	60.2	84.6
TE22	63.7	89.6

# Support bead in airline



$$Z_{airline} = j\eta_0 \frac{f}{f_{ca}} \frac{1}{\sqrt{1 - \left(\frac{f}{f_{ca}}\right)^2}}$$

for  $f < f_{ca}$

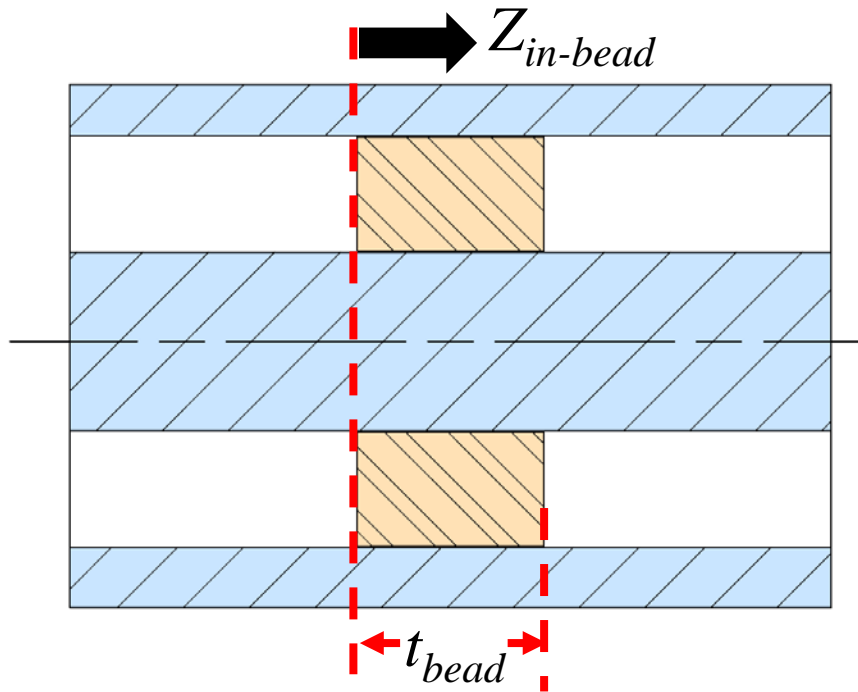
$$\gamma_{airline} = 2\pi \frac{f_{ca}}{c_0} \sqrt{1 - \left(\frac{f}{f_{ca}}\right)^2}$$

where;  $\eta_0 = 376.7$  ohms

$f_{ca} = TE_{11}$  frequency of airline  
 = 19.4 GHz for 7mm line

*Calculate transmission line parameters in terms of TE wave impedance and propagation constant*

# Support bead in airline



$$Z_{in-bead} = Z_{bead} \frac{Z_{airline} + Z_{bead} \tanh(\gamma_{bead} t_{bead})}{Z_{bead} + Z_{airline} \tanh(\gamma_{bead} t_{bead})}$$

where;  $Z_{bead} = \eta_{bead} \frac{1}{\sqrt{1 - \left(\frac{f_{cb}}{f}\right)^2}}$

$$\gamma_{bead} = j2\pi\sqrt{\epsilon_{rb}} \frac{f}{c_0} \sqrt{1 - \left(\frac{f_{cb}}{f}\right)^2}$$

$$\eta_{bead} = \frac{376.7}{\sqrt{\epsilon_{rb}}}$$

$t_{bead}$  = Length of bead

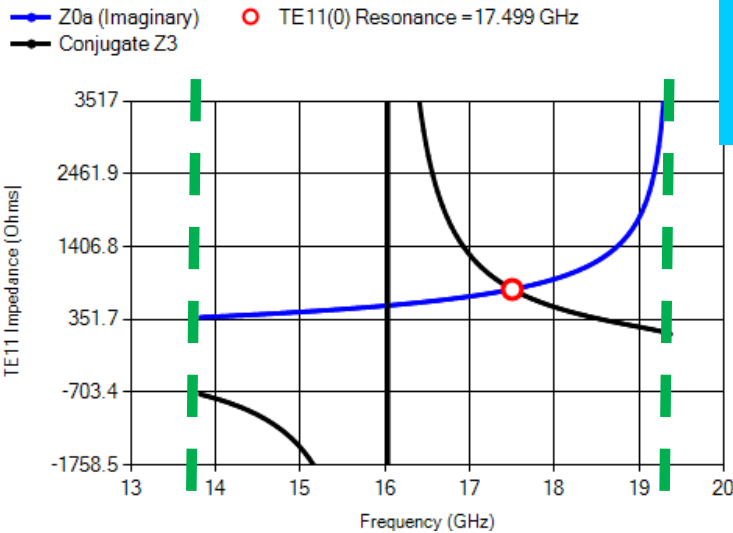
$f_{cb} = TE_{11}$  frequency of bead

= 13.8 GHz for PTFE bead

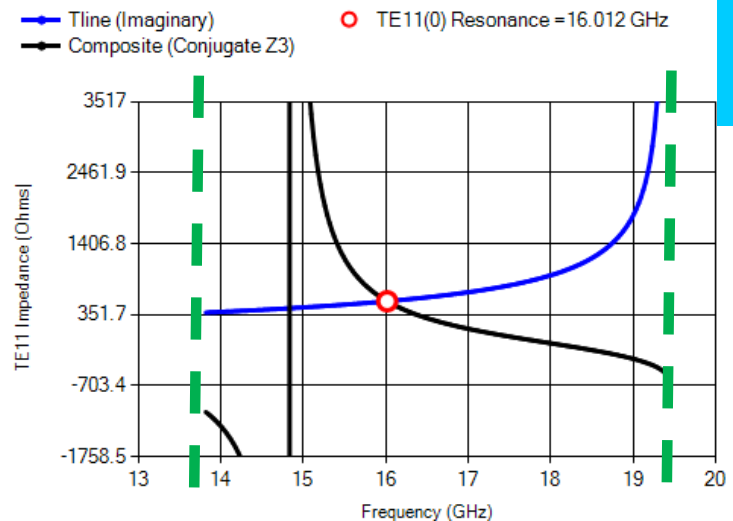
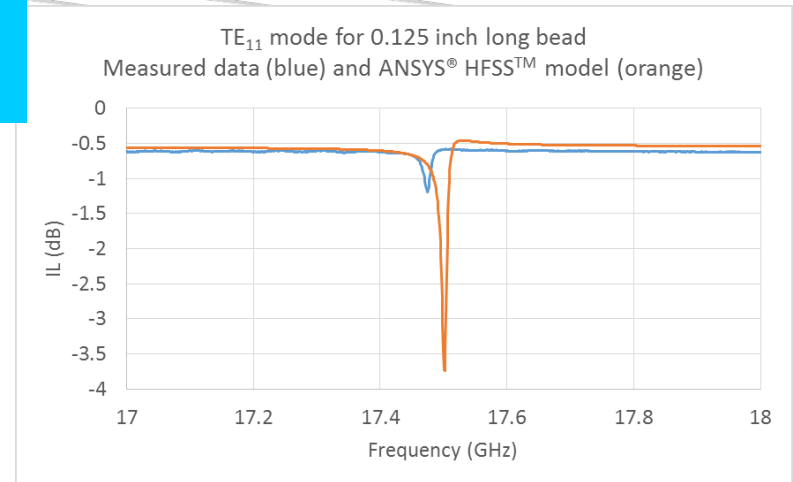
Resonance conditions occur when:

$$Z_{in-bead} = Z_{airline}^*$$

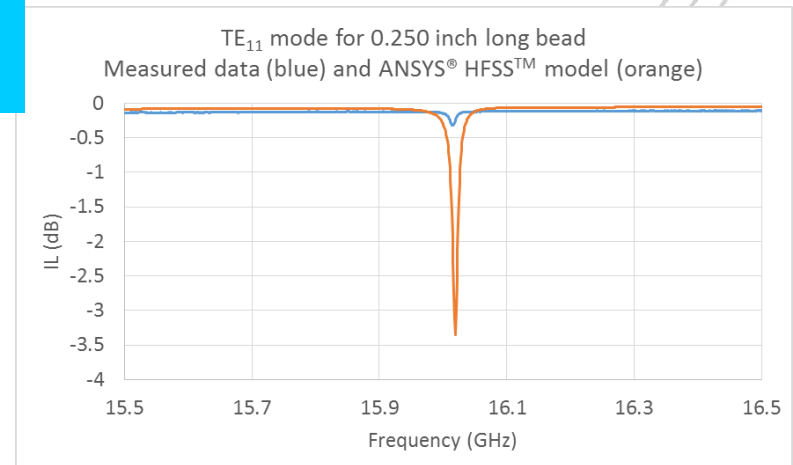
# PTFE bead with 7mm airline experiment



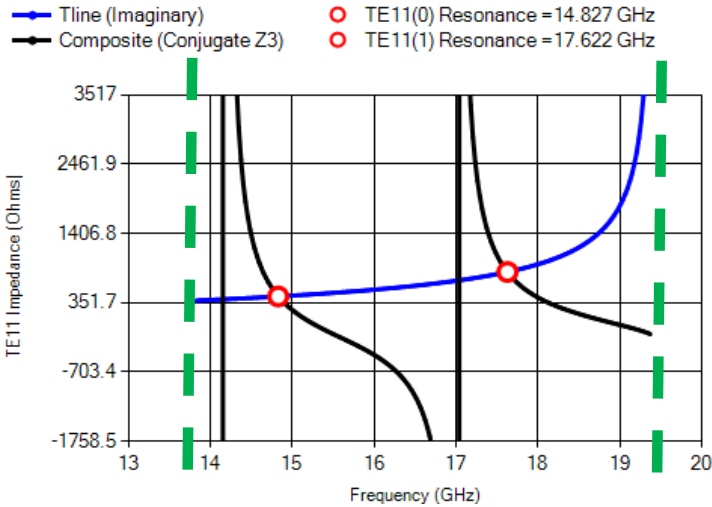
**0.125 inch  
long bead**



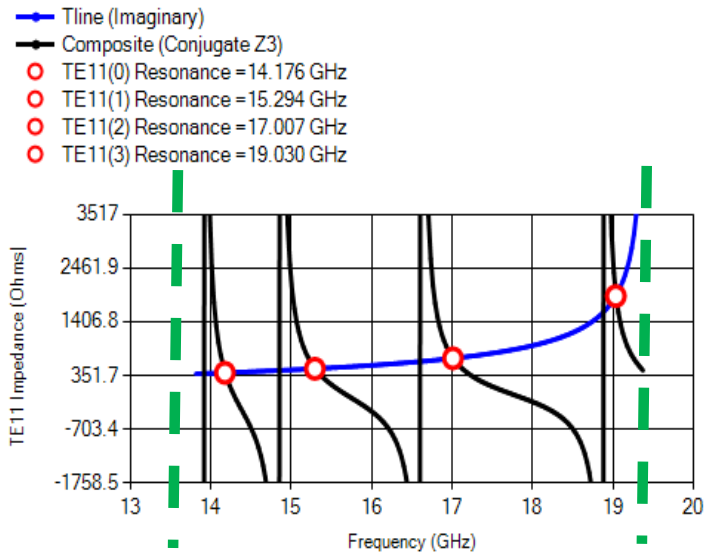
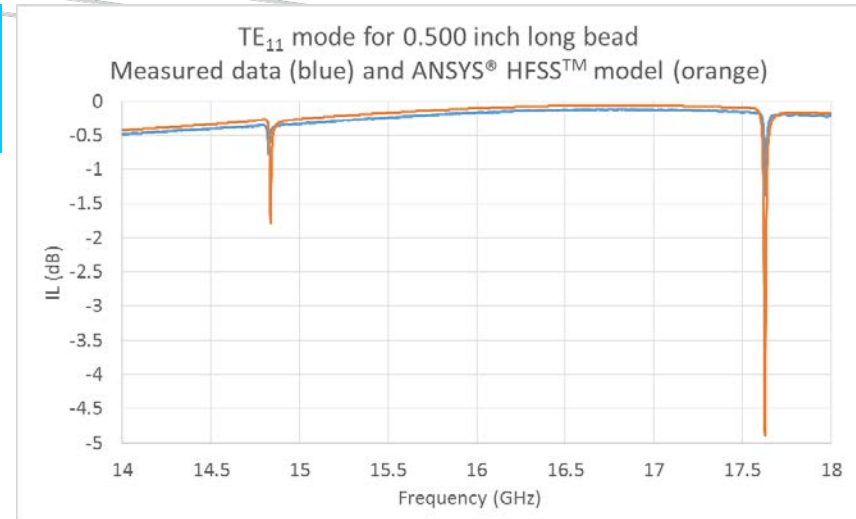
**0.250 inch  
long bead**



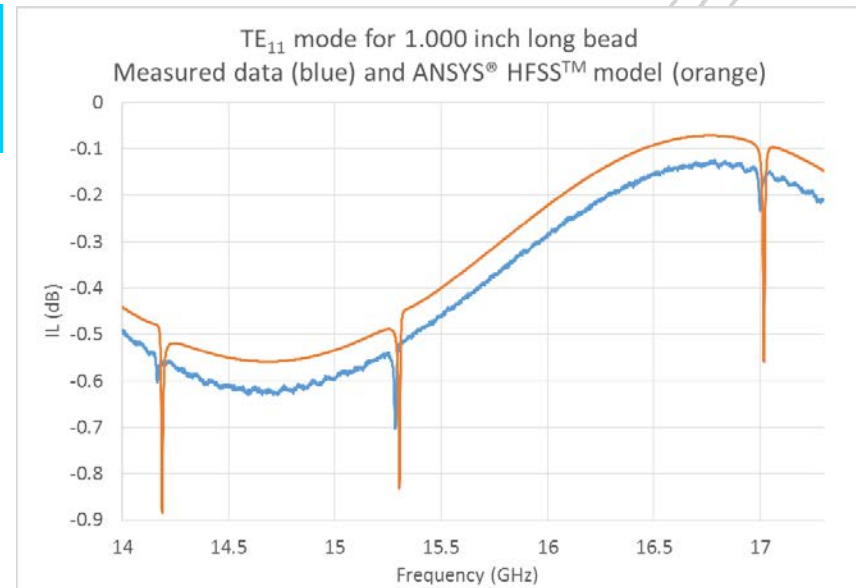
# PTFE bead with 7mm airline experiment



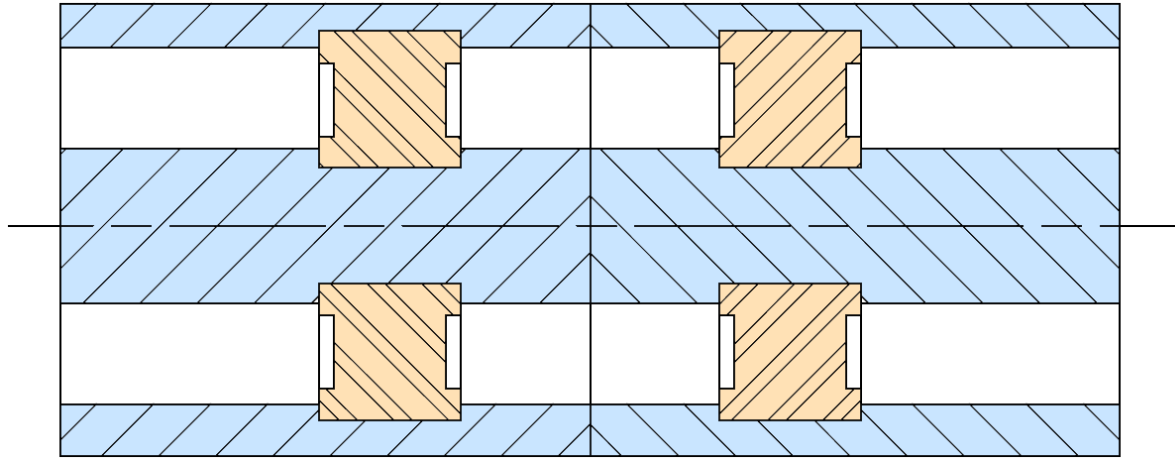
0.5 inch long bead



1.0 inch long bead

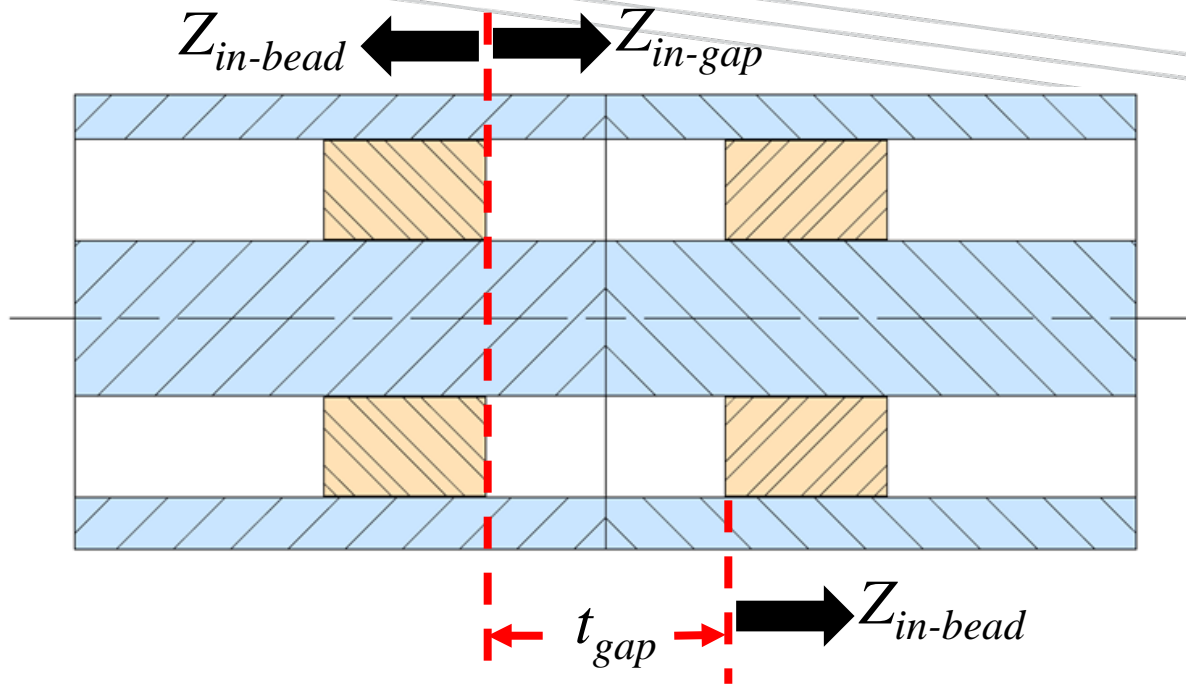


# Dual beads within an airline



Interface between  
two connectors

# Dual beads within an airline



$$Z_{in-gap} = Z_{gap} \frac{Z_{in-bead} + Z_{gap} \tanh(\gamma_{gap} t_{gap})}{Z_{gap} + Z_{in-bead} \tanh(\gamma_{gap} t_{gap})}$$

where;  $Z_{gap} = Z_{airline}$  ;  $\gamma_{gap} = \gamma_{airline}$

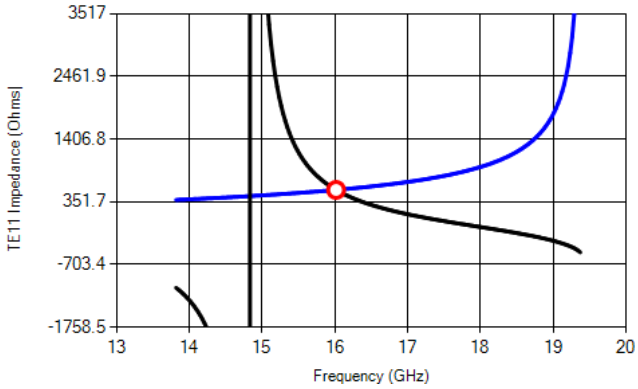
Resonance occurs when:

$$Z_{in-gap} = Z_{in-bead}^*$$

# Dual PTFE beads within 7mm airline

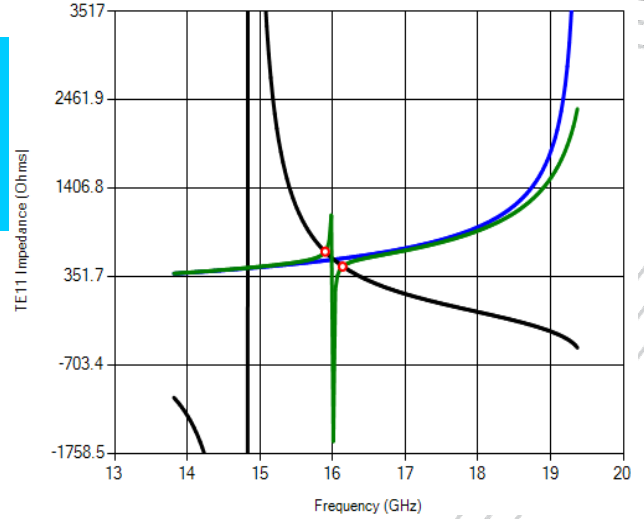
**0.250 inch long single bead**

- Tline (Imaginary)
- Composite (Conjugate Z3)
- TE11(0) Resonance = 16.012 GHz



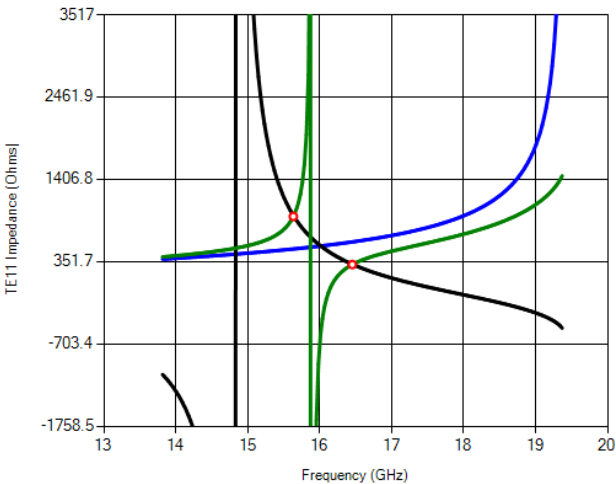
**(2x) 0.250 beads, 0.5 inch apart**

- Tline (Imaginary)
- Composite (Conjugate Z3)
- Gap Space (Imaginary Z4)
- TE11(0:Low) Resonance = 15.896 GHz
- TE11(0:High) Resonance = 16.139 GHz



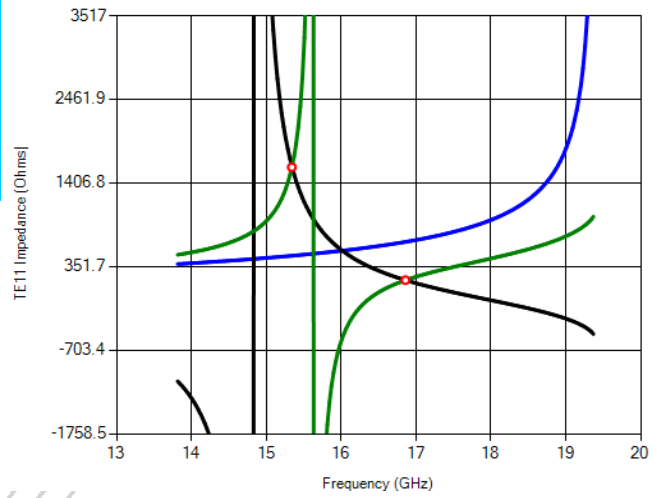
**(2x) 0.250 beads, 0.250 inch apart**

- Tline (Imaginary)
- Composite (Conjugate Z3)
- Gap Space (Imaginary Z4)
- TE11(0:Low) Resonance = 15.636 GHz
- TE11(0:High) Resonance = 16.455 GHz



**(2x) 0.250 beads, 0.125 inch apart**

- Tline (Imaginary)
- Composite (Conjugate Z3)
- Gap Space (Imaginary Z4)
- TE11(0:Low) Resonance = 15.344 GHz
- TE11(0:High) Resonance = 16.857 GHz





## Conclusions:

- Important to understand  $TE_{11}$  mode resonant conditions in order to determine the max operating frequency of coax assembly
  - Use transmission line calculation approach
    - Using TE wave impedance and prop const.
  - Simulate using ANSYS® HFSS™ software
    - Introduce slight asymmetries in geometry
  - Measure the assembly to validate the lowest  $TE_{11}$  resonant frequency